

ANSYS Simulation Results

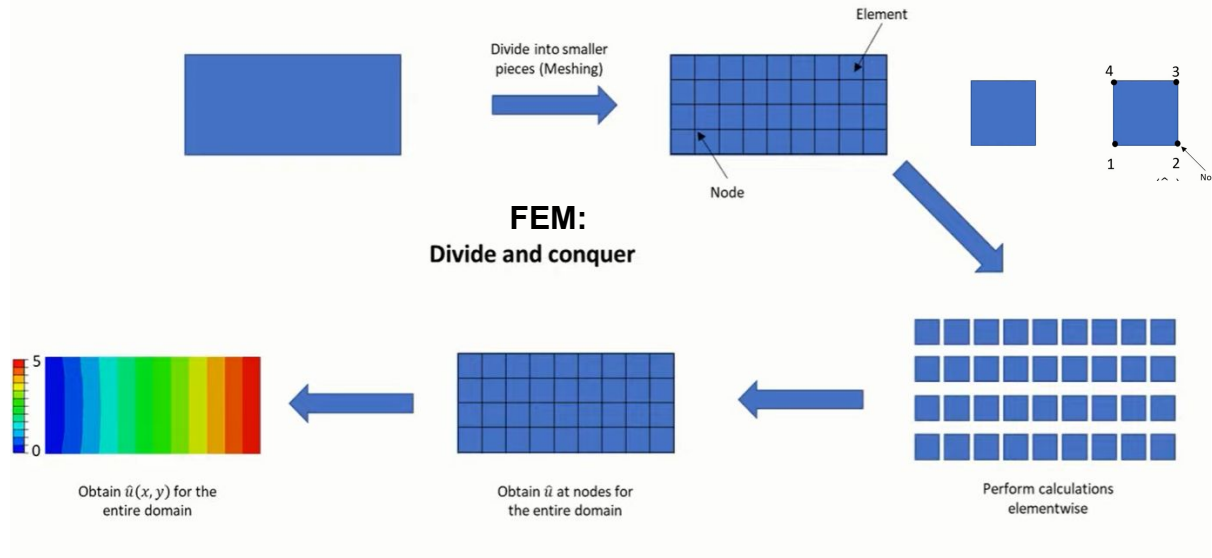
In-Lab Setup and Beampipe Bakeout

By Emma Yeats

Background

Quick Intro to Finite Element Analysis (FEA)

FEA: Utilizes the general Finite Element Method (FEM) to analyze and calculate the solution to boundary value problems on complex 3D geometries.



FEM: obtains an approximate solution to a set of differential equations, boundary conditions by converting the boundary value problem to a system of linear equations.

General steps:

- ❖ Create your complex geometry in ANSYS's CAD software, SpaceClaim
- ❖ Create a mesh

smaller mesh size ↔ more accurate solution ↔ longer computation

- ❖ State initial conditions, materials and domains
- ❖ Initialize and calculate. Then check out your results!

All simulations were solved using ANSYS Fluent software.

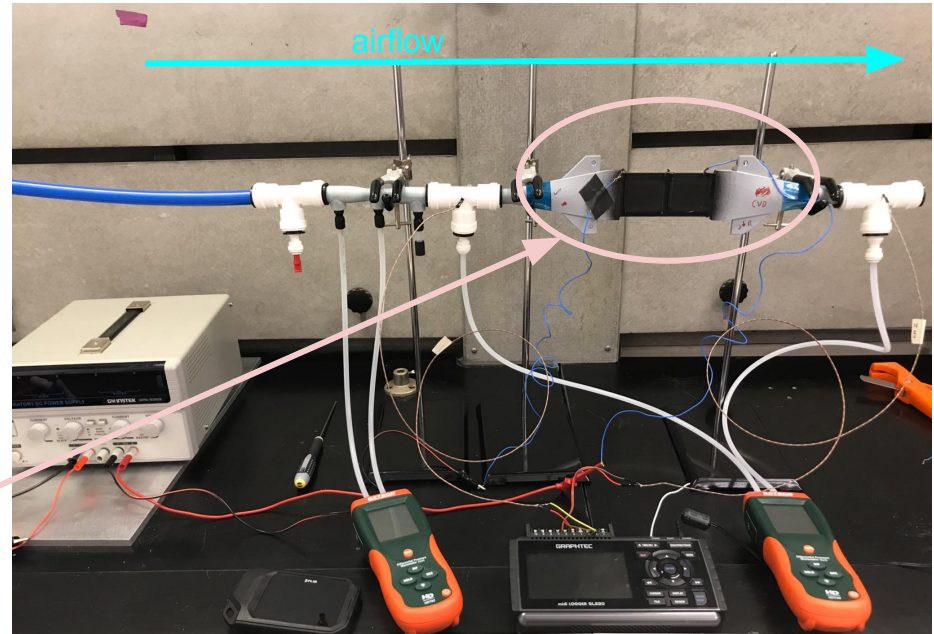
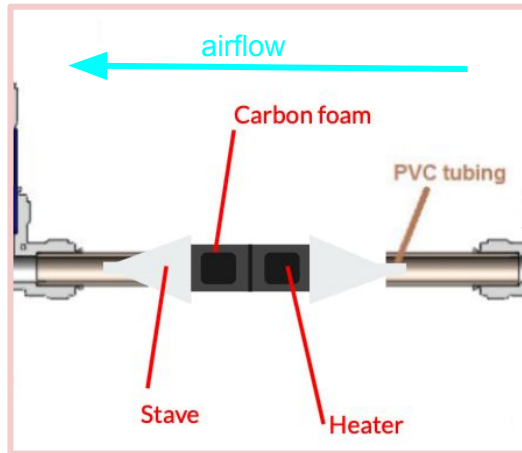
- ❖ Typically used for fluid flow simulations, but we calculated temperature distributions to study the effects of air cooling.

In-Lab Stave Setup

Thermal Simulation

In-Lab Stave Setup

In-lab setup flows air of varying temperature through carbon foam interior to the stave to cool the heater.



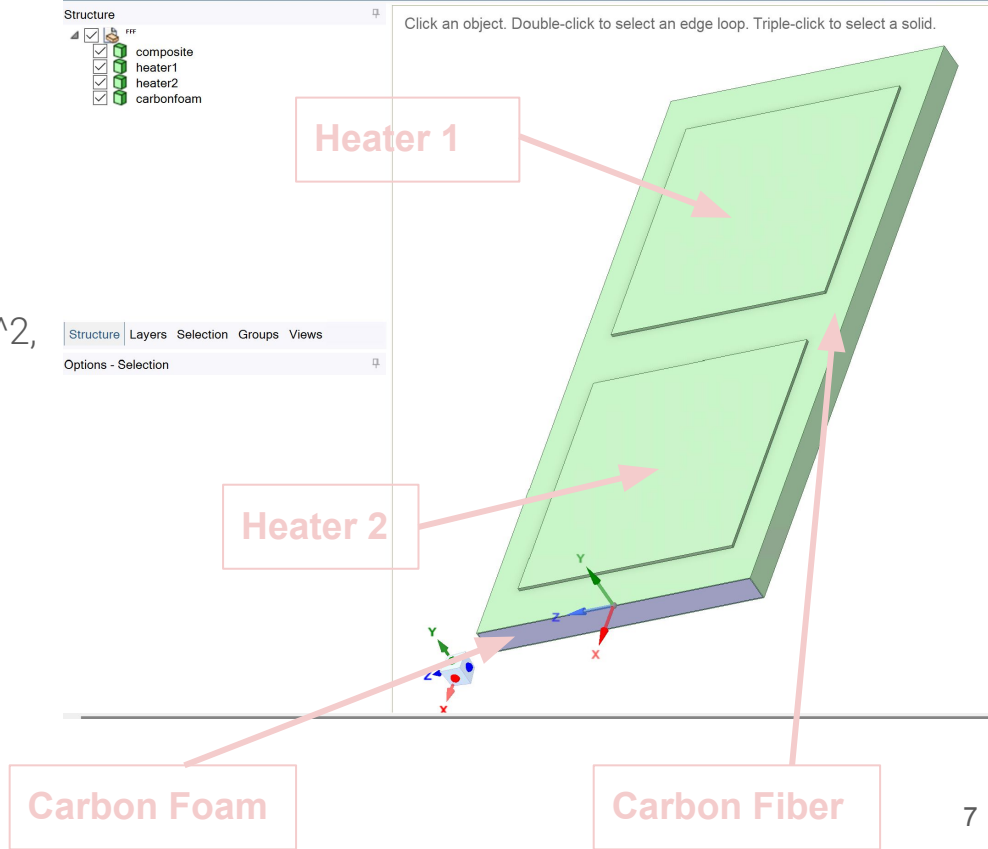
ANSYS Setup

❖ Initial Conditions

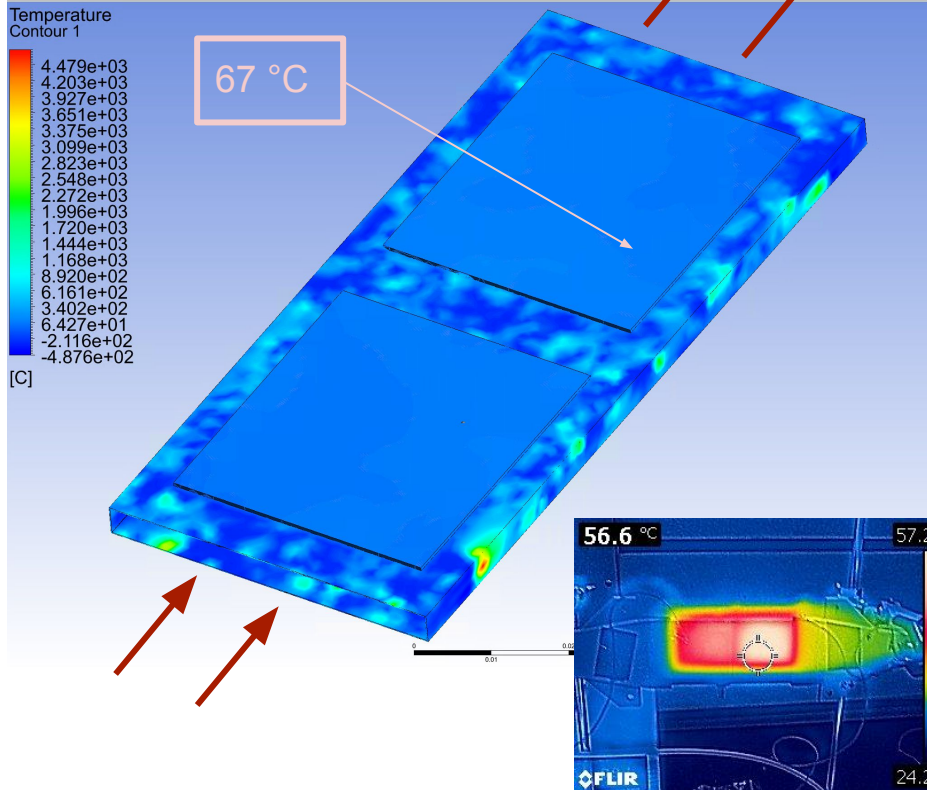
- Heat Output 3000 W/m^2
- Incoming airflow velocity 5 m/s
- Incoming airflow temperature 300 K
- Porous fluid domain with viscous resistance coefficients $K = .4462e+8 \text{ m}^2$, $c = .15$

❖ Materials

- Carbon foam (porous zone)
- Carbon fiber
- Pure silicon



Simulation Results



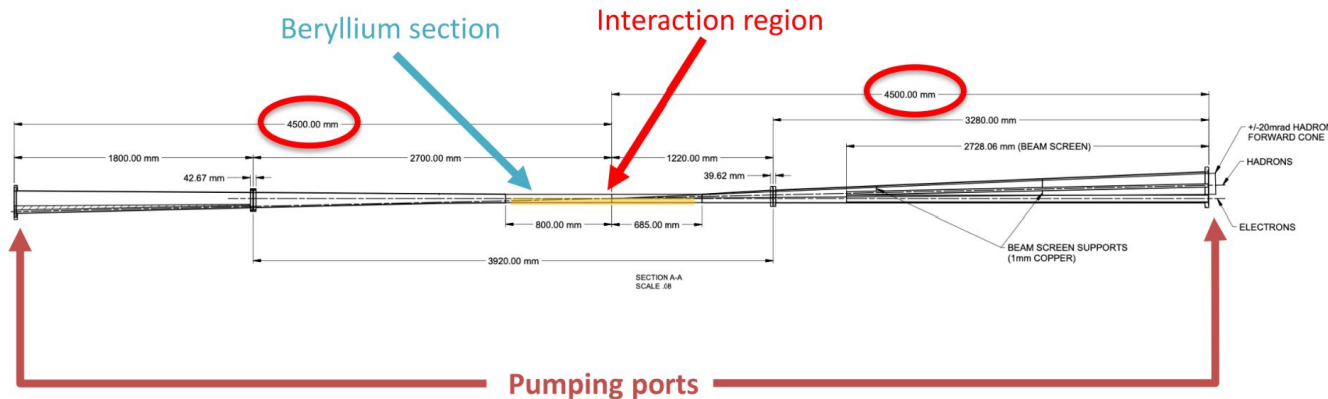
- ❖ Results are close to matching the data found by the in-lab setup.
 - Center of first heater ~ 325 K (51°C)
 - Center of second heater ~ 338 K (65°C)
- ❖ Porous medium coefficients may need to be adjusted
- ❖ Overall, provides a nice benchmark to continue with more air cooling simulations

Beampipe Bakeout

Thermal Simulation

Bakeout Problem

- ❖ We need to remove water molecules and other contaminants from the interior section of the beampipe (beryllium/interaction region).
 - Pump hot gas in, at $\geq 100^\circ\text{C}$, to break water molecule bonds
- ❖ A previous ANSYS study found the minimum distance between Layer1 and the beampipe, $\sim 5\text{mm}$, in order to keep Layer 1 around 30°C but the study neglected the effects of air cooling on the beampipe

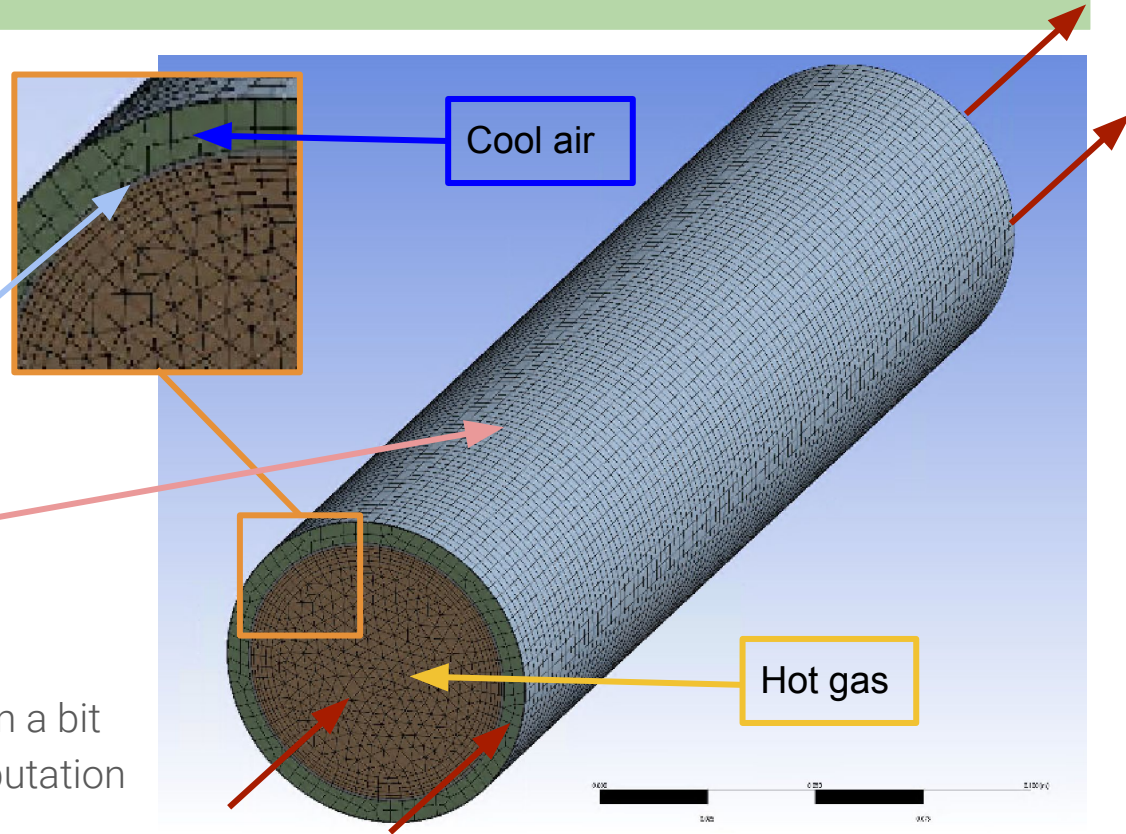


A recent experimental setup had difficulty achieving a gas temperature $\geq 100^\circ\text{C}$

Setup

- ❖ Initial Conditions at Inlet
 - Cool air temperature 298 K
 - Cool air velocity 5 m/s
 - Hot gas velocity 5 m/s
- ❖ Materials
 - Beryllium Alloy
 - Pure silicon

Note: had to make the width of the silicon a bit larger due to limitation in meshing/computation

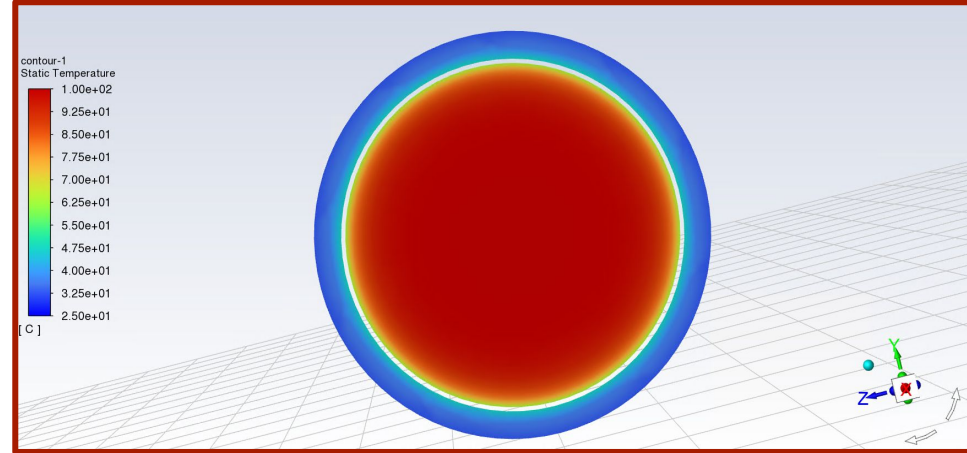
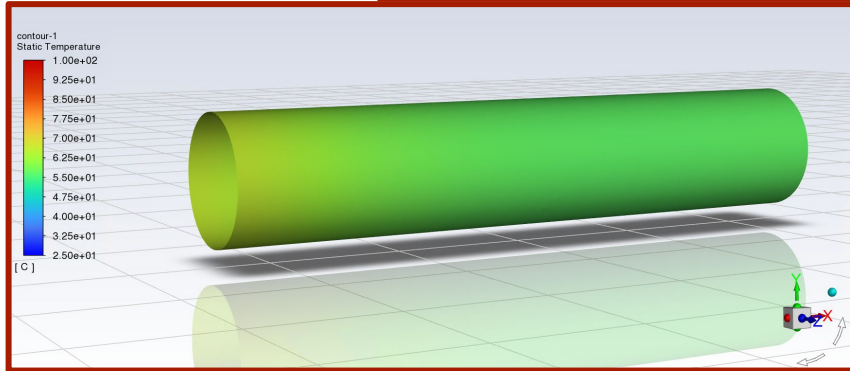


Simulation Results

Inner edge cools significantly
(60-70°C)

Not great!

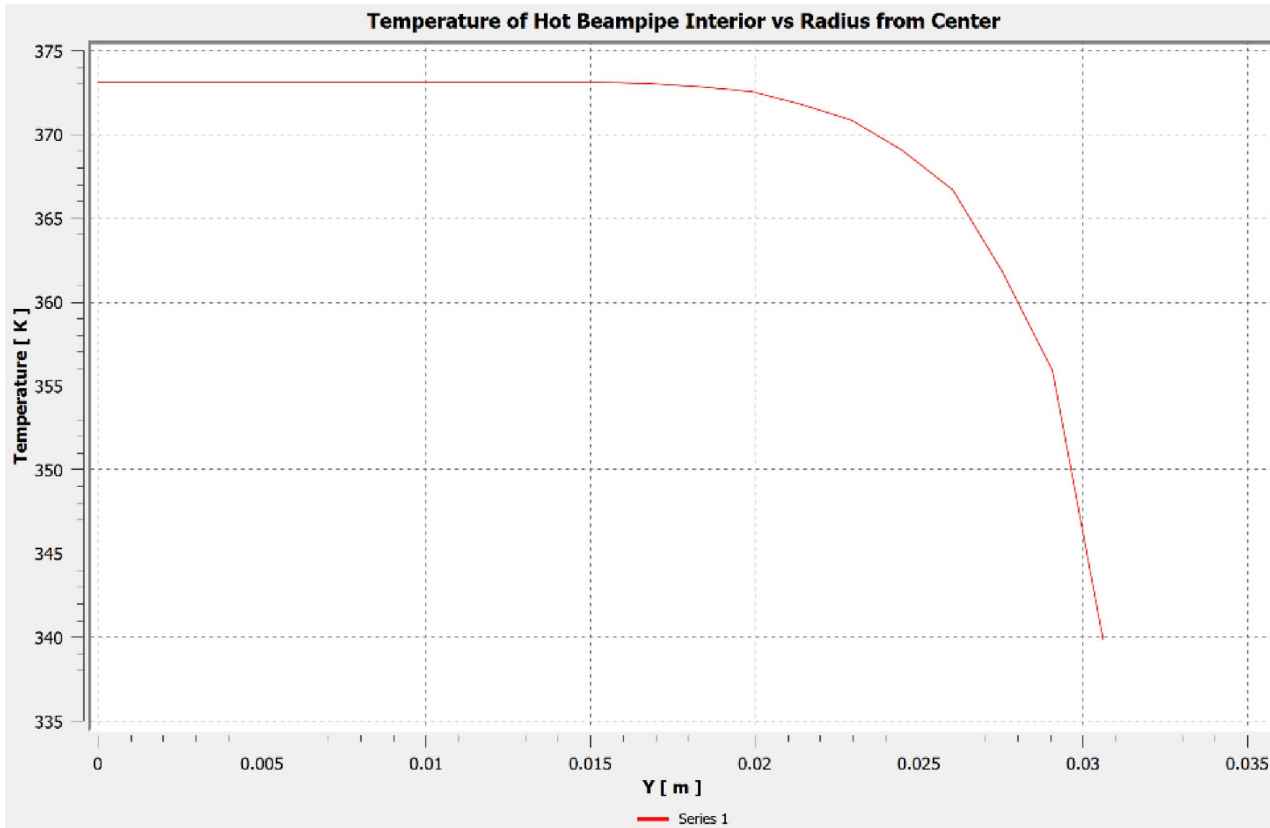
Inner Surface of Beampipe



Beampipe Outlet

Likely need to reoptimize a few parameters, like cooling air velocity, temperature, and hot gas temperature

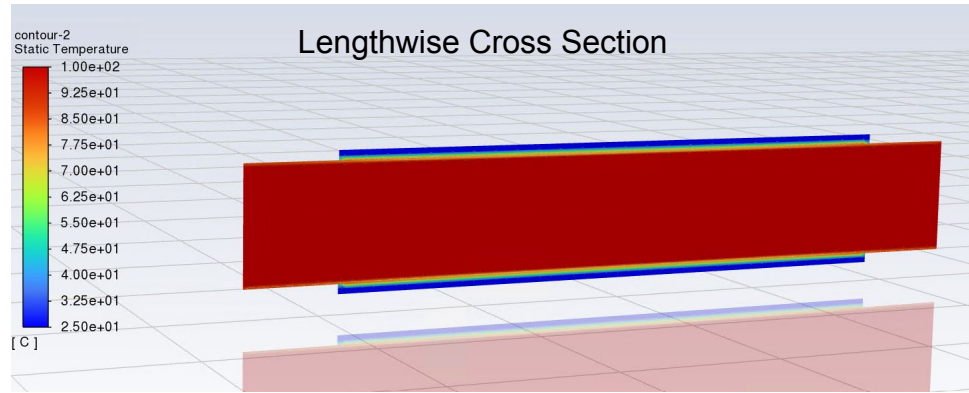
Simulation Results



Sudden drop at edge of beampipe interior (at the outlet).

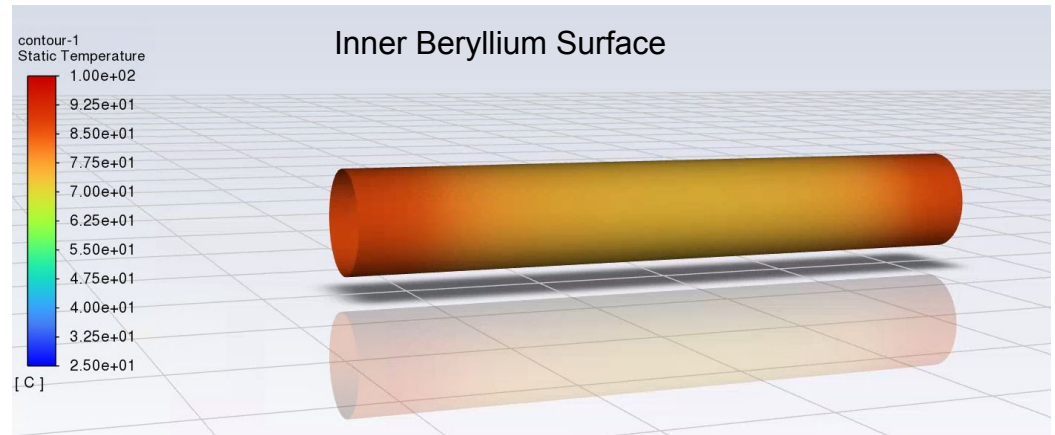
Lowest Temperature is 340 K, or $\sim 67^{\circ}\text{C}$

Back to Basics



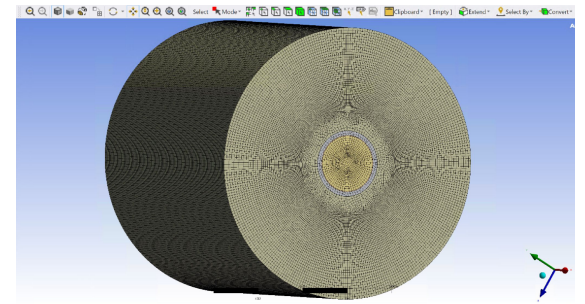
In light of previous results, we wanted to study what would happen if the hot gas was held at constant temperature (100°C) paired with no airflow.

If we can find the minimum hot gas temperature needed to give the beryllium a temperature of 100°C , then our results should mirror JLab's (future work)



Summary + Future Work

- ❖ Verified simulation results with experimental data (in-lab setup)
- ❖ Began study of beampipe bakeout and working towards a more optimized setup
- ❖ What's next?
 - Generally, refine mesh and run more iterations (possible new computer?)
 - Check resistance coefficients for porous medium (carbon foam)
 - Apply air cooling simulation to the barrel and disk components of EIC tracker
 - Include a more accurate geometry of the entire beryllium section of the beampipe
 - Verify type of hot gas used inside
 - Test out different hot gas temperatures
 - Test out different airflow velocities and temperatures

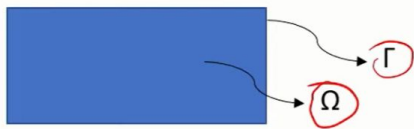


Special Thanks to Youtube Teachers/References

Big shoutout to Ming Zhao on youtube because he's awesome

- ❖ Singularity Engineering
- ❖ CFD Ninja
- ❖ Solid Mechanics Classroom
- ❖ Ansys-Tutor
- ❖ *Thermal and Mechanical Analysis of Carbon Foam* by Mihnea S. Anghelescu
- ❖ *EIC – Thermal Analysis of Beryllium Section of Beampipe* by Pablo Campero

Mathematical treatment



- Poisson's equation:

$$\rightarrow \frac{\partial^2 u}{\partial x^2} + \frac{\partial^2 u}{\partial y^2} = \phi$$

(+ Boundary conditions)

- If $u^e(x,y)$ is an exact solution, then

$$\bullet \frac{\partial^2 u^e}{\partial x^2} + \frac{\partial^2 u^e}{\partial y^2} - \phi = 0$$

- Let \hat{u} is an approximate solution,

$$\bullet \frac{\partial^2 \hat{u}}{\partial x^2} + \frac{\partial^2 \hat{u}}{\partial y^2} - \phi \neq 0$$

$$\bullet \text{Residual } R = \frac{\partial^2 \hat{u}}{\partial x^2} + \frac{\partial^2 \hat{u}}{\partial y^2} - \phi$$

- Now the objective is to find an approximate solution \hat{u} such that R is close to zero at each point within our domain Ω

- Weighted-Residual (WR) statement

$$\bullet \int W(x,y) \left(\frac{\partial^2 \hat{u}}{\partial x^2} + \frac{\partial^2 \hat{u}}{\partial y^2} - \phi \right) d\Omega = 0 \text{ (or)}$$

$$\rightarrow \bullet \int W(x,y) (\nabla^2 \hat{u} - \phi) d\Omega = 0$$

Integrate by parts

- Weak form of the WR statement

$$\bullet \int W \nabla \hat{u} \cdot \hat{n} d\Gamma - \int \nabla W \cdot \nabla \hat{u} d\Omega - \int W \phi d\Omega = 0$$

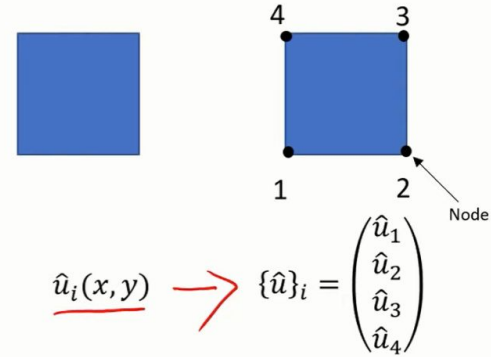
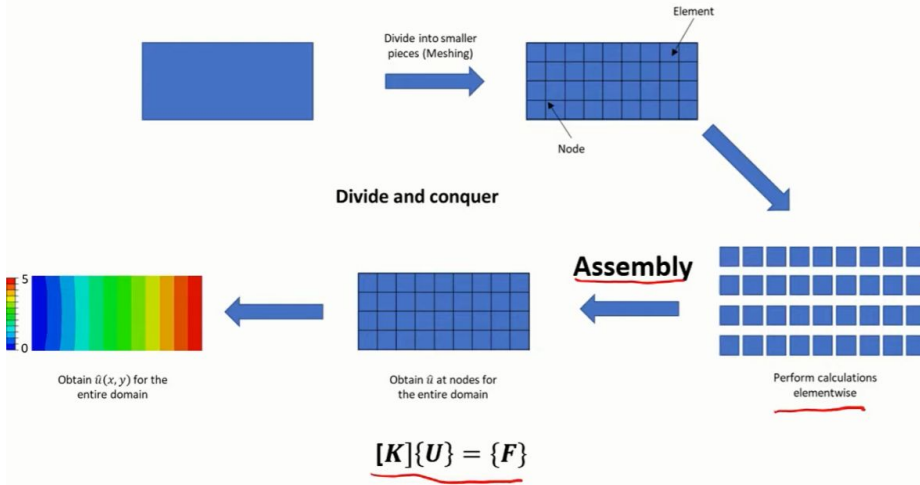
Process of FEM

$$\int W \nabla \hat{u} \cdot \hat{n} \, d\Gamma - \int \nabla W \cdot \nabla \hat{u} \, d\Omega - \int W f \, d\Omega = 0$$

(Defined for entire domain)

$$\int W \nabla \hat{u} \cdot \hat{n} \, d\Gamma_i - \int \nabla W \cdot \nabla \hat{u} \, d\Omega_i - \int W f \, d\Omega_i = 0$$

(Defined for each element)



$$\hat{u}(x,y) = N_1(x,y) \hat{u}_1 + N_2(x,y) \hat{u}_2 + N_3(x,y) \hat{u}_3 + N_4(x,y) \hat{u}_4$$

(OR) $\hat{u}(x,y) = \sum N_k u_k$ or $[N]\{u\}$

substitute

$$\rightarrow \int W \nabla \hat{u} \cdot \hat{n} \, d\Gamma - \int \nabla W \cdot \nabla \hat{u} \, d\Omega - \int W f \, d\Omega = 0$$

$\rightarrow [k]_i \{u\}_i = \{f\}_i$