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## Transverse stress test of two Bi-2212 Rutherford cables

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US MDP zoom meeting, 19th of July 2023

### Motivation: stress in Bi-2212 dipole magnets

### 80 to 105 MPa azimuthal stress present in recent high-field Bi-2212 dipole magnet designs

- Apart from one early date test, there are no systematic test data existing on cables
- It would be useful to have experimental data on stress limits for recent Bi-2212 cables



Results are also highly relevant for high-field solenoids under high radial compressive load!

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#### **Bi-2212 Rutherford cable**



#### Cable press in 11 T solenoid



- Bi-2212 samples and test setup
- Sample preparation
- Transverse stress results
- Microstructural analysis of cable ross-sections
- Conclusion

### **Bi-2212 Rutherford cable samples**

• Two sample were tested at Uni. Twente in transverse stress set-up:

Zhang et al. (2018), <u>https://doi.org/10.1088/1361-6668/aada2f</u> LBNL 17-strand Bi-2212 Rutherford Cable Mullite braided insulation Bi-2212



0.8

mm

	Sample 3	Sample 4
Cable no.	LBNL1109	LBNL2002
Number of strands	17	17
Size excl. insulation	7.8 mm x 1.4 mm	7.8 mm x 1.4 mm
Twist pitch	58 mm	58 mm
Bi-2212 wire	Nontwisted PMM180207_4, 5, 6 ,7, 55x18, 0.8mm, Engi-mat powder LXB103	PMM190118, 55x18, 0.8mm, Engi-mat LXB156
Insulation	Mullite sleeve, 150 µm thick	Mullite sleeve, 150 µm thick
Test date at Uni. Twente	December 2022	June 2023

Wire cross-section (Zhang et al.)



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# Sample holder 11 T solenoid Press coils Image by Boschman et al. https://doi.org/10.1109/20.133551

TO TRANSFORMER

### Transverse stress setup

- 50 kA superconducting transformer
- 11 T solenoid magnet
- 250 kN press
- 4.2 K helium bath

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50 kA transformer



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# Sample after heat treatment

Stainless steel reaction holder

Bi-2212 Rutherford \_ cable in mullite sleeve

#### Pictures of sample 4 after heat treatment



The samples were heat treated at NHMFL in 49:1 mixture of argon and oxygen with a total gas pressure of 50 bar (892°C)



### **Epoxy impregnation**

- Vacuum impregnation with CTD-101k at 60°C, 0.6-0.8 mBar
- Cured for 5 hour at 110°C and 16 hour at 125°C in a furnace

#### Sample surface after heat treatment



Impregnation setup Vacuum chamber Rod for moving the sample Sample holder Heated resin container

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50 cm

### Pushing block and strain gauges





- Block glued onto the sample with Stycast 2850FT/23LV and three layers of glass ribbon
- Pushed area is 8.1 mm x 45 mm = 3.654 cm<sup>2</sup>



- Strain gauge (CFLA-6-350-17) on each side of the pushing block
- Attached with cyano-acrylate glue (TMI CN)

### Sample connection to the transformer



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### **Initial** VI curves

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### T = 4.2 K, $B_a = 11$ T, σ = 10 MPa

- Voltage measured on 6 strands and current leads; they all look smooth and consistent
- Voltage criterion of 4.5  $\mu$ V results from  $E_c = 10^{-4}$  V/m and 45 mm pushing block length



### Initial I<sub>c</sub>(B) curve

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### **Comparison of samples:**

- Sample 3: LBNL1109, tested Dec 2022
- Sample 4: LBNL2002, tested June 2023
- Engineering current density at 5 T applied field using 7.8 mm<sup>2</sup> cross-sectional area is: 422 A/mm<sup>2</sup> for sample 3, 650 A/mm<sup>2</sup> for sample 4 (54% increase)
- *n*-values are 14 to 15 for both samples and all applied fields in the range 5 to 11 T.



### Critical current versus transverse stress

Applied field 11 T, data normalized to initial  $I_c$  of 2.70 kA (sample 3), and 4.07 kA (sample 4)

- Measurement sequence:
  - 10 MPa
  - 20 MPa
  - 10 MPa
  - 30 MPa
  - 10 MPa
  - 40 MPa
  - etc.
- 5% degradation reached at:

170-200 MPa in sample 3 and 120-150 MPa in sample 4



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### Comparison of the two samples 3 and 4



#### Sample comparison

- Sample 3: LBNL1109, tested Dec 2022
- Sample 4: LBNL2002, tested June 2023

Stronger stress dependence observed in sample 4, at 150 MPa:

- Sample 3 has 3% degradation, whereas
- Sample 4 has 6% degradation
- The difference between the samples at 100 MPa is 1.5% and at 150 MPa is 3% only
- Globally, from a magnet application point of view, the samples behave practically the same.

**Critical current as function of transverse stress** 



### $I_{\rm c}(B)$ curves after applying 200 MPa

#### Sample 3: LBNL1109 (December 2022)

- 7 to 8% field-independent  $I_c$  reduction
- *n*-value dropped by 1 to 2 points



### Sample 4: LBNL2002 (June 2023)

- 12 to 13% field-independent *I*<sub>c</sub> reduction
- *n*-value dropped by 2 to 3 points



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### Effect of mechanical load cycling 10 to 200 MPa

#### Sample 3: LBNL1109 (December 2022)

- 2.5% *I*<sub>c</sub> reduction after 50 cycles
- No significant change in *n*-value

#### Sample 4: LBNL2002 (June 2023)

- 3.6% reduction after 50 cycles
- 4.6% reduction after 200 cycles
- No significant change in *n*-value



Load cycling I<sub>c</sub> reduction at 200 MPa is modest (some 5 %), and saturating (good).

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# Microstructural analysis cross-sections of sample 3 OF TWENTE.



- 5 cross-sections examined (200 MPa, 8% *I*<sub>c</sub> decrease)
- No obvious damage seen yet, main degrading cause not yet identified
- I<sub>c</sub>-degradation = broken current path + some residual stress redistribution effect
- In Nb<sub>3</sub>Sn we see filament  $\mu$ m-cracking, current in entire filament interrupted
- May be here (hypothesis, for discussion) we brake with nm-cracking current path at grain boundaries mainly on surface of filaments, not leading to global cracking.....
- Sample 4 has seen 300 MPa and -45%, next to be examined....



### Conclusion

- Results obtained on 2 Bi-2212 cable samples, another 2 to be tested
- Initial whole cable critical current density at 5 T applied field was 422 A/mm<sup>2</sup> in sample 3 (LBNL1109) and 650 A/mm<sup>2</sup> in sample 4 (LBNL2002)
- 5% critical current decrease reached at an average transverse stress of 170 to 200 MPa in sample 3 and at 120 to 150 MPa in sample 4
- Progressive I<sub>c</sub> reduction (but saturating) observed in both samples when cycling between 10 and 200 MPa
- All changes in critical current were irreversible



